Abstract: Investigations of processes occurring during wastewater treatment have progressed beyond the stage of technology. Currently, great numbers of representatives of diverse specialist research apply increasingly sophisticated measurement methods that have not been employed in this field of science. One of the methods is IRMS (Isotope Ratio Mass Spectrometry). Tracking changes in the ratios of biogenic element isotopes is useful in eg identification and monitoring of investigated processes. Since the IRMS technique has hardly been used for investigations of the wastewater treatment process, pilot research should be instigated to determine the isotope ratios occurring naturally in the process. The aim of the study was to determine changes in carbon and nitrogen isotope ratios at the successive stages of the technological line in wastewater treatment plants. The study material comprised: i) suspensions of raw sewage and mixtures of wastewater and activated sludge; ii) gases sampled from the volume of the suspensions; iii) gases sampled from the air above the suspension surface. The research material originated from the facilities of “Hajdow” municipal wastewater treatment plant in Lublin (SE Poland). The samples were analysed for the carbon and nitrogen isotope ratios, and the concentrations of the gases as well as total organic carbon (TOC), inorganic carbon (IC), Kjeldahl nitrogen (KN), dry weight, pH, and Eh were determined. The results obtained suggest that: i) the IRMS technique can be successfully applied in investigations of processes occurring during wastewater treatment; ii) isotope ratios in the carbon and nitrogen compounds (CO$_2$ and N$_2$) both in the suspensions and gases contained therein and in the air above them differ from each other and change at the different stages of the treatment process; iii) further research is indispensable in order to identify processes responsible for fractionation of carbon and nitrogen isotopes.

Keywords: IRMS, stable isotopes, wastewater, activated sludge, gas emission
the wastewater treatment plant [3-5], the structure of the communities [6-8], the mechanical properties of flocs [9-10], or the colour of sludge [11]. Important and widely discussed task in the area of wastewater treatment are the ways of physiological activity of activated sludge description, expressed by eg different types of OUR (Oxygen Uptake Rate) [12-14] and fractioning of the substrate for building and calibration of models of sewage treatment processes eg models of ASM group [12, 14-17]. Investigations of the agricultural use of wastewater are equally important [18-21].

As it is visible above, mostly there are determined sewage parameters treated in the particular facilities of WWTP and properties of activated sludge. But for gases that are formed in treatment plant mainly odour nuisances are considered from the engineering and scientific point of view [22-24]. These problems are solved in most of cases by objects encapsulation and directing of the smelling gases through proper filters, eg biofilters. Since a short time it is taken into consideration emission of greenhouse gases from WWTP [25, 26], and the possibility to valuate wastewater treatment process or quality of treated sewage basing on gaseous substances emitted from wastewater [27, 28].

One of the methods widely used in environmental studies other than analyses of the wastewater treatment process is the IRMS (Isotope Ratio Mass Spectrometry) technique [29-32]. It consists in separation of different isotopes in a constant, strong electromagnetic field, which allows determination of stable isotope ratios in a sample (eg $^{13}$C and $^{12}$C as well as $^{15}$N and $^{14}$N) [33].

Literature does not provide many papers on the application of the IRMS technique in analysis of wastewater treatment processes or, more broadly, investigations of the impact of wastewater on the environment. The few authors describing these issues should be mentioned: i) Ronkanen and Kløve [34], who investigated the process of wastewater treatment in peatlands; ii) Law et al [35], who quantified the proportion of C isotopes in raw sewage and subsequent distribution of the element after primary and secondary treatment processes; iii) Zvab Rozic et al [36], who used the IRMS technique to detect dispersal of pollution along the Adriatic Sea coast; iv) Morriss ey et al [37], who used stable isotopes as indicators of the impact of wastewater on organisms inhabiting urban rivers; v) Lindehoff et al [38], who determined the effect of municipal sewage on the toxicity of selected algal species; or vi) Gammons et al [39], who focused on nitrogen and carbon transformations in a small watercourse, where municipal wastewater was discharged [34-39]. Yet, there are no reports presenting the values of stable isotope ratios for wastewater and/or sludge at different stages of treatment.

A comprehensive IRMS-based analysis of processes occurring in wastewater treatment plants necessitates assessment of the background, which in the context of the proposed research involves determination of isotope ratios at successive stages of the technological process in a wastewater treatment plant. The aim of this study was to perform a preliminary assessment of changes in the $\delta^{15}$N and $\delta^{13}$C content in wastewater, sludge, and gases emitted into the atmosphere at subsequent stages of the technological system in a wastewater treatment plant.
Materials and methods

Wastewater samples and analyses

Material for the analyses was sampled from technological system facilities at the mechanical-biological wastewater treatment plant “Hajdow”, Lublin (central-eastern Poland), which removes carbon, nitrogen and phosphorus compounds with the average mean capacity of 65,000 m$^3$/d. Sanitary and industrial sewage from Lublin agglomeration are discharged to the wastewater treatment plant, where they are purified in the following facilities: bar screen primary sedimentation tanks - pumping stations - anaerobic chambers - main bioreactors (for nitrification, denitrification and biological dephosphatation processes) - secondary sedimentation tanks. Biological part of WWTP is based on modified BARDENPHO system. The investigation was performed using gas and liquid samples.

Two types of gas samples were collected: the air above the chambers and gas emitted in the volume of the wastewater and activated sludge mixture. Gases from ambient air were sampled with a syringe, whose inlet was placed ca. 20 cm above the surface of the wastewater and activated sludge mixture. The gas was stored in gas-tight vessels. Gas released in the volume of the wastewater and activated sludge mixture was sampled by means of loaded chambers immersed upside down. Gases produced as a result of microbial activity moved in the sludge towards its surface and accumulated in the chambers, thereby forcing the chambers to emerge on the surface. The gases were sampled into gas-tight vessels with the use of a syringe. They were taken from the sludge at each of the below presented stages, except for the raw sewage (no possibility of sampling).

The liquid samples comprised raw wastewater entering the treatment plant and the sewage and activated sludge mixture. They were kept in 250 cm$^3$ bottles.

The gas and liquid samples were taken at the same successive points of the following facilities of technological line:
1 - inlet - raw sewage;
2 - bioreactor: denitrification chamber I - wastewater and activated sludge;
3 - bioreactor: nitrification chamber I - wastewater and activated sludge;
4 - bioreactor: denitrification chamber II - wastewater and activated sludge;
5 - bioreactor: nitrification chamber II - wastewater and activated sludge;
6 - recirculate - thickened activated sludge.

The sampled mixtures of wastewater and activated sludge were well stirred and subjected to physico-chemical analyses in order to assess the content of total organic carbon, inorganic carbon (IC), Kjeldahl nitrogen, dry weight, pH, and Eh.

TOC and IC were determined using an automated Shimadzu TOC-V CPH carbon analyser coupled with an SSM 5000 A attachment in accordance with manufacturer’s instructions. KN was determined with the use of a Behr Labor-Technik instrument in accordance with the attached application note. The dry matter content was determined on the basis of the PN -EN 12879:2004 standard. The values of pH and Eh were determined with a Hach-Lange HQ 40D multi-measure device using electrodes Intellical PHC and Intellical ORP.

The dry weight (of the liquid samples) was analysed in order to determine the stable carbon isotope ratios ($^{13}$C relative to $^{12}$C) and nitrogen ($^{15}$N relative to $^{14}$N). The sample preparation procedure was as follows: 8 mg of dry weight (dried at 105ºC) was mixed with 1 g of copper oxide (CuO) and ground in a mortar. Next, the mixture was placed in oxygen-
purged glass tubes (pyrex glass) and a few chips of pure copper were added. The next step was tube-sinking with a gas burner and incineration in a furnace at a temperature of 560ºC for 8 hours. Incinerated samples were purified under vacuum to remove water and other contaminants. The samples were analysed for the content of isotopes δ\(^{13}\)C and δ\(^{15}\)N separately. The measurements were performed in the Mass Spectrometry Laboratory, Institute of Physics, Maria Curie-Sklodowska University, Lublin (Poland) using a triple-collector mass spectrometer with a dual-inlet system. The δ\(^{13}\)C was measured according to PDB using NBS-22 and IA-R042 (powdered bovine liver), while the δ\(^{15}\)N using IA-R042. Atmospheric nitrogen was the standard for the nitrogen compounds. The standard uncertainty rate was 0.05‰.

The gas samples were assessed for the concentrations of CO\(_2\), O\(_2\), and CH\(_4\). The analysis was performed using a Shimadzu GC- 14A gas chromatograph equipped with a Thermo Conduction Detector (TCD) with helium as a carrier gas. The CO\(_2\) and CH\(_4\) concentrations were analysed using a steel column packed with Porapak Q, whereas the O\(_2\) concentration was assessed on a column packed with a molecular sieve 5A. 0.1 cm\(^3\) of gas was loaded into the column each time.

Analysis of the carbon isotopic composition of carbon dioxide was performed in the gas samples using a stable isotope ratio mass spectrometer (IRMS - Isotope Ratio Mass Spectrometry) Thermo Electronics DELTA V Advantage with a continuous gas flow. 0.1 cm\(^3\) of gas was dispensed. The δ\(^{13}\)C was measured according to PDB. The standard uncertainty rate was 0.05‰.

For the GC and IRMS analyses, the samples were dispensed using a syringe with a manual feeder (with a stop-valve) and a conically tipped 0.1 cm\(^3\) VICI needle with a side port, which prevented mixing the sampled gas with laboratory air.

All measurements (both physico-chemical analyses and stable isotope ratio assessment) were done in triplicate.

Calculations and statistical analysis

Isotope data are expressed in the δ notation defined as the relative difference between the isotope ratio in the sample and the standard. The δ\(X\) values are expressed as [40]:

\[
\delta X = ((R_{sample} / R_{standard}) - 1) \cdot 1000 \text{ [‰]}
\]

where: \(X\) is \(^{13}\)C or \(^{15}\)N, \(R_{sample}\) is the isotope ratio (\(^{13}\)C/\(^{12}\)C or \(^{15}\)N/\(^{14}\)N) of the sample, and \(R_{standard}\) is the isotope ratio (\(^{13}\)C/\(^{12}\)C or \(^{15}\)N/\(^{14}\)N) of the standard (PDB-Pee Dee Bellemnite for C, atmospheric N\(_2\) for N) [41].

Results and discussion

The physico-chemical characteristics of the tested suspensions are presented in Table 1. The values presented in Table 1 as well as the information provided by the technologist indicate that on the day of sampling the wastewater treatment plant worked without failure and purified the wastewater efficiently.

The concentrations of methane, carbon dioxide, and oxygen in the analysed gas samples are shown in Figures 1 and 2.

In the gases sampled from the volume of the wastewater and activated sludge mixture, methane was detected at all the sampling points, except for nitrification chamber I.
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The highest concentration was recorded in the anaerobic denitrification chamber (sampling point 2).

The concentrations of carbon dioxide and oxygen in samples taken from the volume of the wastewater and activated sludge mixture were correlated with each other. The highest concentration of oxygen was noted in nitrification chamber I (sampling point 3), where the CO$_2$ concentration was the lowest and no methane was detected. A relatively high concentration of oxygen (8.52%) was recorded in nitrification chamber II. In the other samples, the oxygen concentration ranged from 2.47 to 5.46%.

Physicochemical characteristics of the suspensions at the successive sampling points

<table>
<thead>
<tr>
<th>Sampling point</th>
<th>Dry mass [g/kg]</th>
<th>pH</th>
<th>Eh  [mV]</th>
<th>TOC [g/dm$^3$]</th>
<th>TKN [g/dm$^3$]</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>0.84</td>
<td>6.94</td>
<td>–392.67</td>
<td>0.18</td>
<td>0.08</td>
</tr>
<tr>
<td>2</td>
<td>2.52</td>
<td>6.93</td>
<td>–305.50</td>
<td>0.29</td>
<td>0.27</td>
</tr>
<tr>
<td>3</td>
<td>2.80</td>
<td>6.89</td>
<td>–178.80</td>
<td>0.29</td>
<td>0.29</td>
</tr>
<tr>
<td>4</td>
<td>2.88</td>
<td>6.85</td>
<td>–227.00</td>
<td>0.32</td>
<td>0.29</td>
</tr>
<tr>
<td>5</td>
<td>3.10</td>
<td>6.76</td>
<td>–178.00</td>
<td>0.31</td>
<td>0.28</td>
</tr>
<tr>
<td>6</td>
<td>6.55</td>
<td>6.71</td>
<td>–218.00</td>
<td>0.50</td>
<td>0.63</td>
</tr>
</tbody>
</table>

Fig. 1. Concentrations of methane (A), carbon dioxide (B) and oxygen (C) in gas samples emitted from the volume of the mixture of wastewater and activated sludge

Fig. 2. Concentrations of methane (A), carbon dioxide (B) and oxygen (C) in air sampled above the suspension surface
No gas sample taken from above the suspension surface (except for that taken at the inlet) contained methane (Fig. 2A). In the air samples taken above raw sewage, the CH$_4$ concentration was approximately 100 fold higher than that in the ambient atmospheric air in this part of Europe, which currently is 1.8 ppm.

The concentration of carbon dioxide (Fig. 2B) in all the gas samples taken from headspace (except for the gases from above raw sewage) ranged from 0.12 to 0.18%. The lowest concentration was noted above the recirculate (sampling point 6). The concentrations were several-fold higher than those in the ambient atmospheric air in this part of Europe. The concentration of CO$_2$ above the surface of raw sewage (sampling point 1) was nearly 5 times higher than in the other sampling points and reached 0.86%.

The analyses of the carbon isotopic composition of CO$_2$ revealed that all the samples had a lower content of the heavier isotope than CO$_2$ contained in the atmospheric air from this region of Poland; at the height of 2 m above the ground, ambient $\delta^{13}$C of CO$_2$ ranges from $-7.56$ to $-18.56‰$ depending on the time of the day [42]. Simultaneously, carbon dioxide in the samples taken from the air above the suspension (Fig. 3A) contained significantly lower amounts of the heavier C isotope than CO$_2$ sampled from the volume of the wastewater and activated sludge mixture (Fig. 3B). The values of the carbon isotopes in CO$_2$ from air sampled above the surface of the suspension at the various treatment stages ranged from $-33$ to $-46‰$, whereas the range of the values of $\delta^{13}$C of CO$_2$ in the air sampled from the volume of the wastewater and activated sludge mixture was narrower, $ie$ $-22$ to $-29‰$.

The values of $\delta^{13}$C of CO$_2$ sampled from the volume of the wastewater and activated sludge mixture (Fig. 3B) exhibit certain regularity: CO$_2$ emitted in the denitrification chambers (anaerobic conditions or limited oxygen availability - sampling points 2 and 4) contained higher quantities of isotope $^{13}$C than in the nitrification chambers characterised by oxygen availability (sampling points 3 and 5). $\delta^{13}$C of CO$_2$ in the recirculate (sampling point
6) was increased, compared to the value obtained for nitrification chamber II, *i.e.* the content of the heavier isotope increased.

![Fig. 4. Values of δ¹³C of carbon dioxide (A) and δ¹⁵N of N₂ (B) for the dry weight of the sludge in the respective sampling points](image)

The highest value of δ¹³C (hence, the highest content of the heavier isotope) in the solid samples (Fig. 4A) was noted in sampling point 1, *i.e.* prior to the treatment process. In the subsequent purification steps, substantial differences in the delta values are noticeable. It is worth noting that the values of δ¹³C CO₂ for the dry weight of sludge (Fig. 4A) are closer to the δ¹³C CO₂ values determined in gases sampled from the suspensions rather than to the δ¹³C CO₂ values recorded for gases collected above the suspension surface.

The analysis of the δ¹⁵N values recorded at the successive stages of the wastewater treatment process shows a clearly increasing tendency for the δ¹⁵N value (hence, an increase in content of the heavier ¹⁵N nitrogen). Additionally, the analysis of the successive processes (denitrification chamber → nitrification chamber → denitrification chamber → nitrification chamber; sampling points 2-5) reveals a similar relationship as in the case of carbon: the anaerobic conversion of the nitrogen compounds increased the content of the heavier ¹⁵N isotope, and the aerobic processes were accompanied by a decreased content of δ¹⁵N. This phenomenon may be related to the fractionation process or “mixing” of activated sludge from the different sampling points.

At this stage of the research, it is difficult to elucidate the course of carbon and nitrogen fractionation in the wastewater treatment process. As already mentioned, the present investigations are a preliminary step, and further research is indispensable to answer the question why deltas increase in some processes and decrease in others. However, occurrence of fractionation has already been confirmed. Therefore, one can claim that the IRMS technique can be successfully applied for analyses of purification processes.

Since we failed to find literature reports of the δ¹⁵N and δ¹³C values for raw sewage or activated sludge, it was impossible to compare our results with literature data.
Conclusions

1. The IRMS technique can be successfully used in investigations of processes occurring during sewage treatment.

2. The isotope ratios in carbon and nitrogen (CO\textsubscript{2} and N\textsubscript{2}) compounds in suspensions and gases contained therein as well as in the ambient air differ from each other and change in the respective stages of the purification process.

3. Further research is indispensable for identification of processes responsible for fractionation of carbon and nitrogen isotopes within facilities of WWTP.

References

Changes of isotopic composition in gases emitted from wastewater treatment plant - preliminary study


**ZMIANY SKŁADU IZOTOPOWEGO GAZÓW EMITOWANYCH Z Oczyszczalni Ścieków - Badania Wstępne**

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**Abstrakt:** Badania procesów zachodzących w trakcie oczyszczania ścieków dawno wyszły już poza fazę technologiczną. Obecnie zaobserwować można coraz większe grono przedstawicieli różnych specjalności wykorzystujących do badań coraz bardziej wyszukane metody pomiarowe, które do tej pory nie były wykorzystywane w tym obszarze. Jedną z takich metod jest IRMS (Isotope Ratio Mass Spectrometry). Sledzenie zmian stosunków izotopów pierwiastków biogenicznych jest przydane m.in. w identyfikacji i monitorowaniu badanych procesów. Ponieważ technika IRMS praktycznie nie była do tej por y wykorzystywana do badania procesu oczyszczania ścieków, dlatego niezbędne są pilotażowe badania pozwalające na wyznaczenie naturalnie występujących stosunków izotopowych w tym procesie. Celem pracy było określenie zmian stosunków izotopów węgla i azotu na wybranych stopniach ciągu technologicznego oczyszczalni ścieków. Materiał badawczy obejmował: i) zawiesziny ścieków surowych i mieszaniny ścieków i osadu czynnego, ii) próbki gazów z objętości zawiesin; iii) próbki gazów z powietrza sponad powierzchni zawiesin. Materiał badawczy pochodził z miejskiej oczyszczalni ścieków „Hajdów” w Lublinie (SE Polska). Próbki analizowano pod kątem stosunków izotopów stabilnych węgla i azotu, stężeń gazów oraz zawartości całkowitego węgla organicznego (TOC), węgla nieorganicznego (IC), azotu Kjeldaha (KN), suchej masy, pH i Eh. Uzyskane wyniki sugerują, że: i) technika IRMS może być z powodzeniem stosowana w badaniach procesów zachodzących podczas oczyszczania ścieków, ii) stosunki izotopowe w związkach węgla i azotu (CO\(_2\) i N\(_2\)), zarówno w zawiesinach, jak i w zawartych w nich gazach oraz w powietrzu nad zawiesiną, różnią się od siebie i zmieniają się na różnych etapach procesu obróbki, iii), niezbędne są dalsze badania w celu określenia procesów odpowiedzialnych za frakcjonowania izotopów węgla i azotu.

**Słowa kluczowe:** IRMS, izotopy stabilne, ścieki, osad czynny, emisja gazów